Replacement of Bridge 29 (SR-87 Over Lagoon Creek)

Geotechnical Data Report

Haywood County, Tennessee

August 15, 2025 | Terracon Project No. 1A255072

Prepared for:

American Structurepoint Inc. 600 Superior Ave East, Suite 2401 Cleveland, Ohio 44114





1922 Old Murfreesboro Pike, Bldg 900, Ste 905
Nashville, TN 37217
P (615) 333-6444
Terracon.com

August 15, 2025

American Structurepoint Inc. 600 Superior Ave East, Suite 2401 Cleveland, Ohio 44114

Attn: Mr. Gabe Liptak, P.E.

P: (216) 302-3694

E: gliptak@structurepoint.com

Re: Geotechnical Data Report

Replacement of Bridge 29 (SR-87 Over Lagoon Creek)

Haywood County, Tennessee Terracon Project No. 1A255072

Dear Mr. Liptak:

We have completed the scope of work for the above referenced project. This Data Report presents the findings of the subsurface exploration, including field and laboratory test results.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or if we may be of further service, please contact us.

Sincerely,

Terracon

Eric Conway, P.E.

Geotechnical Department Manager

James Vinson, P.E. National Manager

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Introduction

This report presents the results of our subsurface exploration performed for the proposed bridge replacement along SR-87 in Haywood County, Tennessee. The geotechnical Scope of Services included the advancement of test borings, laboratory testing, geophysical testing and preparation of this data report. The exploratory locations were determined by Terracon field staff. Encountered soil and groundwater depths are provided herein.

Site Information

The following description of site conditions is derived from our site visit in association with field exploration and our review of publicly available geologic and topographic maps.

Item	Description
Site Information	The approximate coordinates for the bridge crossing are as follows: • Bridge No. 29: 35.6310° N 89.4110° W See Site Location
Current Ground Cover	Away from the existing bridge, SR-87 pavement consists of asphalt overlaying fill.
Existing Topography (Estimated using Google Earth)	The ground surface elevation at the borings is approximately 298 feet.

Geologic Formations

Formation ¹	Description				
Alluvial Deposits	Sand, silt, clay, and gravel. Flood plain of the Mississippi River, more than 100 feet thick.				
•	Tennessee, published by the State of Tennessee nservation, Division of Geology (1966).				

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Geotechnical Borings and Laboratory Testing

Terracon drilled two borings near the proposed bridge replacement. Each boring encountered asphalt over fill over alluvial deposits.

Subsurface conditions observed at each location are indicated on the individual logs. The individual logs can be found in the **Exploration Results**. Drawings depicting site locations and boring locations relative to existing site features are attached.

Laboratory testing was performed to confirm visual descriptions and further characterize the encountered soils. Testing included the following: natural moisture, grain-size distribution, Atterberg limits, compaction, California Bearing Ratio, unconsolidated-undrained triaxial and corrosion series. Test results are attached with the boring logs.

Seismic Survey

Terracon performed a limited seismic survey consisting of twenty-two Multi-Channel Analysis of Surface Waves (MASW) arrays at the subject bridge site to obtain shear wave velocities of the soil within the upper 100 feet. Results of the seismic survey as well as location map for the arrays are attached.

General Comments

This geotechnical data report does not include any analysis or recommendations. The data presented in this report are based upon the geotechnical borings and geophysical data at the indicated locations. This report does not reflect variations that may occur across the site, or due to the modifying effects of weather. The nature and extent of such variations may not become evident until, during, or after construction.

No warranties, either expressed or implied, are intended or made. The scope of geotechnical services does not include either specifically or by implication any environmental assessment of the site or identification or prevention of pollutants, hazardous materials, or conditions.

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Attachments

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Exploration and Testing Procedures

Field Exploration

Number of Exploration Points	Approximate Exploration Depth (feet)	Location
2	100	Bridge Abutments
2 MASW Arrays	100	Bridge Abutments

Boring Layout and Elevations: Terracon personnel provided the boring layout using handheld GPS equipment (estimated horizontal accuracy of about ± 10 feet) and referencing existing site features. Approximate ground surface elevations were estimated using Google EarthTM.

Subsurface Exploration Procedures: We advanced the borings with an truck-mounted rotary drill rig using continuous flight solid stem augers and rotary wash boring techniques as necessary depending on soil conditions. Three samples were obtained in the upper 10 feet of each boring and at intervals of 5 feet thereafter. In the thin-walled tube sampling procedure, a thin-walled, seamless steel tube with a sharp cutting edge was pushed hydraulically into the soil to obtain a relatively undisturbed sample. In the split-barrel sampling procedure, a standard 2-inch outer diameter split-barrel sampling spoon was driven into the ground by a 140-pound automatic hammer falling a distance of 30 inches. The number of blows required to advance the sampling spoon the last 12 inches of a normal 18-inch penetration is recorded as the Standard Penetration Test (SPT) resistance value. The SPT resistance values, also referred to as N-values, are indicated on the boring logs at the test depths.

We also observed the boreholes while drilling with augers for the presence of groundwater. The measured groundwater levels are shown on the attached boring logs.

The sampling depths, penetration distances, and other sampling information was recorded on the field boring logs. The samples were placed in appropriate containers and taken to our soil laboratory for testing and classification by a Geotechnical Engineer. Our exploration team prepared field boring logs as part of the drilling operations. These field logs included visual classifications of the materials observed during drilling and our interpretation of the subsurface conditions between samples. Final boring logs were prepared from the field logs. The final boring logs represent the Geotechnical Engineer's interpretation of the field logs and include modifications based on observations and tests of the samples in our laboratory.

Multi-Channel Analysis of Surface Waves: Our method of investigation utilized a standard fixed-array set of MASW geophones. Each array consisted of 24 4.5Hz

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geophones, spaced 10 feet apart along a sensor cable. For the passive surveys, ambient noise (such as nearby traffic or construction) on the site was recorded by a seismograph. For the active surveys, three sledgehammer strikes were performed every 10 feet against a polyethylene plate from 20 feet before the start of the array through geophone 12.

The data was returned to our office and processed using dispersion analysis software (SurfSeis, engineered by the Kansas Geological Survey) that extracts the fundamental-mode dispersion curve(s). The active and passive surveys performed at each line were combined to produce a broader-band overtone image to better identify the dispersion trends. The resulting curves were inverted and modeled to yield a 1D shear-wave velocity profile along the array to 100 feet below ground surface. The velocity models from the MASW surveys are presented on **Exhibit 2**.

Laboratory Testing

The project engineer reviewed the field data and assigned laboratory tests. The laboratory testing program included the following types of tests:

- Moisture Content
- Unconfined Compression
- Atterberg Limits
- Triaxial Compression
- Grain Size Analysis
- Corrosion Suite
- Standard Proctor
- California Bearing Ratio

Based on the results of our field and laboratory programs, we described and classified the soil samples in accordance with the Unified Soil Classification System.

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Site Location and Exploration Plans

Contents:

Site Location Plan Exploration Plan

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Site Location



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Exploration Plan



Replacement of Bridge 29 (SR-87 Over Lagoon Creek) | Haywood County, Tennessee August 15, 2025 | Terracon Project No. 1A255072

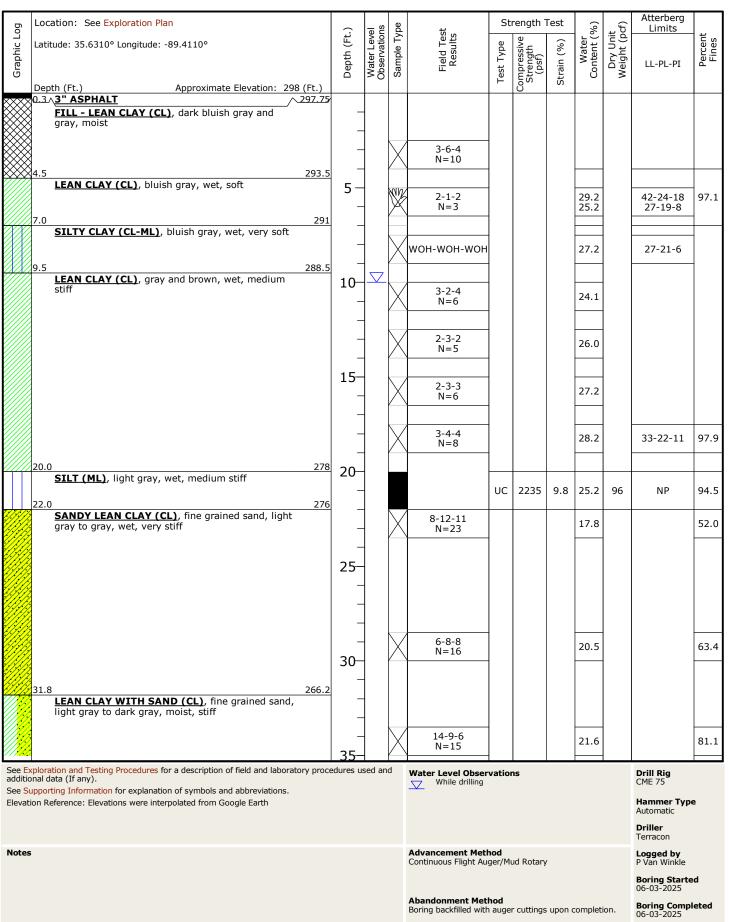


Exploration and Laboratory Results

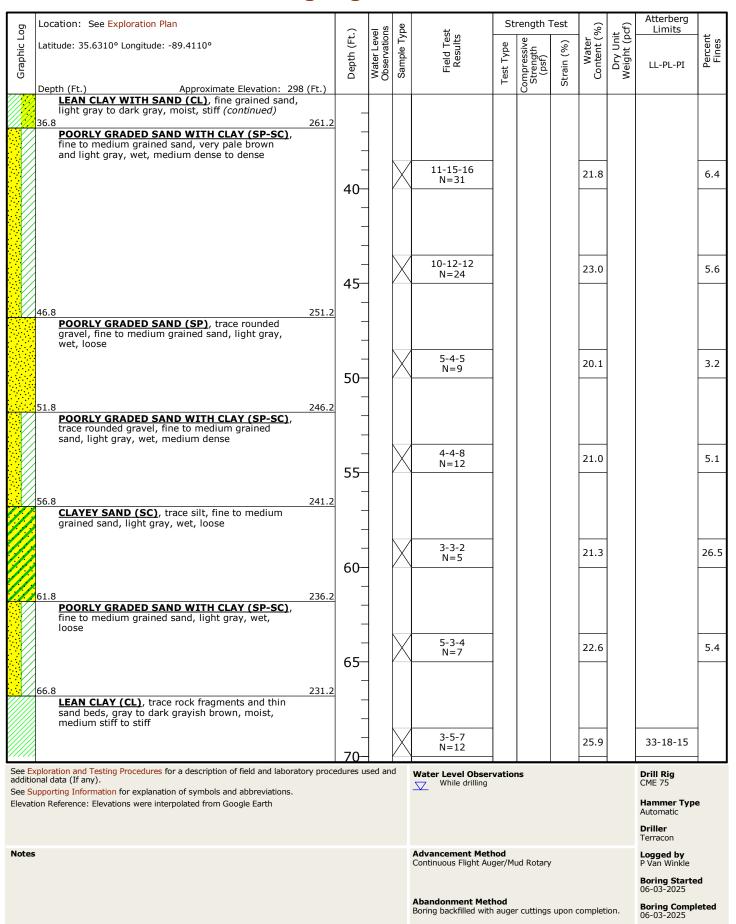
Contents:

Boring Logs (B-29-1 and B-29-2)
Lab Summary
Atterberg Limits
California Bearing Ratio
Standard Proctor
Grain Size Analysis
Triaxial Compression
Corrosion Suite
Geophysical Exploration Results

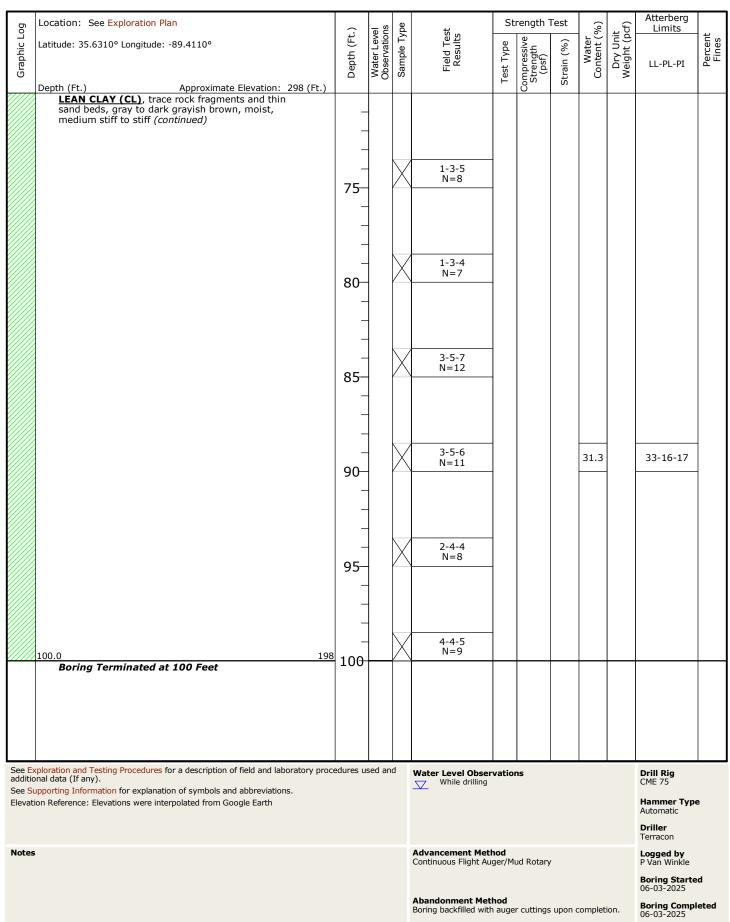




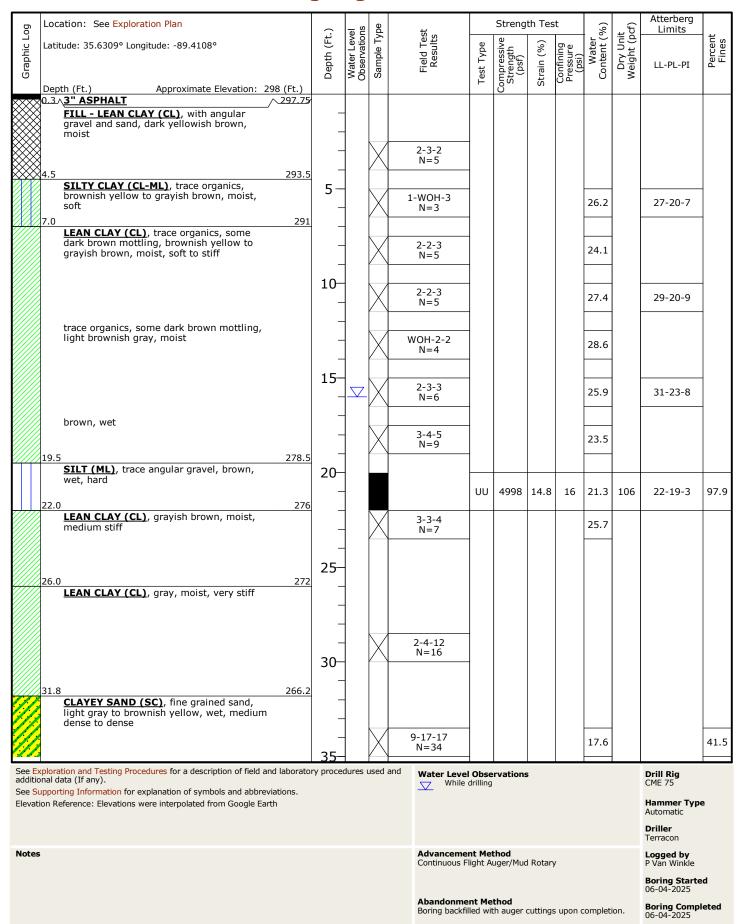




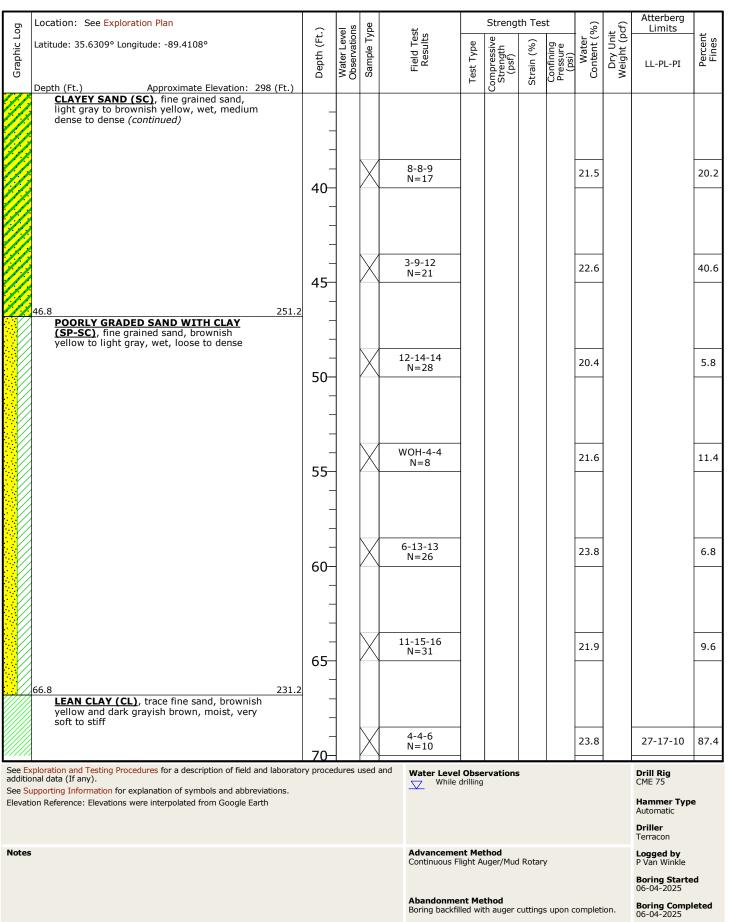




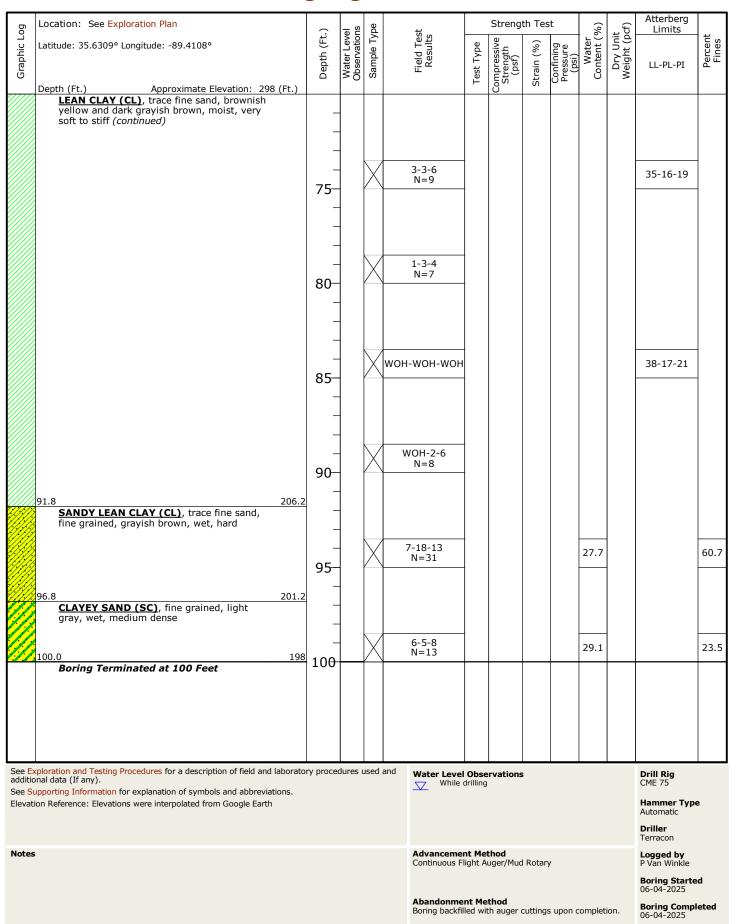














Summary of Laboratory Results

Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity % Fines Index		Water Content (%)
B-29-1	4-7	42	24	18	97.1	29.2
B-29-1	5-6.5	27	19	8		25.2
B-29-1	7.5-9	27	21	6		27.2
B-29-1	10-11.5					24.1
B-29-1	12.5-14					26.0
B-29-1	15-16.5					27.2
B-29-1	17.5-19	33	22	11	97.9	28.2
B-29-1	20-22	NP	NP	NP	94.5	25.2
B-29-1	22-23.5				52.0	17.8
B-29-1	28.5-30				63.4	20.5
B-29-1	33.5-35				81.1	21.6
B-29-1	38.5-40				6.4	21.8
B-29-1	43.5-45				5.6	23.0
B-29-1	48.5-50				3.2	20.1
B-29-1	53.5-55				5.1	21.0
B-29-1	58.5-60				26.5	21.3
B-29-1	63.5-65				5.4	22.6
B-29-1	68.5-70	33	18	15		25.9
B-29-1	88.5-90	33	16	17		31.3



Summary of Laboratory Results

Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity Index	% Fines	Water Content (%)
B-29-2	5-6.5	27	20	7		26.2
B-29-2	7.5-9					24.1
B-29-2	10-11.5	29	20	9		27.4
B-29-2	12.5-14					28.6
B-29-2	15-16.5	31	23	8		25.9
B-29-2	17.5-19					23.5
B-29-2	20-22	22	19	3	97.9	21.3
B-29-2	22-23.5					25.7
B-29-2	33.5-35				41.5	17.6
B-29-2	38.5-40				20.2	21.5
B-29-2	43.5-45				40.6	22.6
B-29-2	48.5-50				5.8	20.4
B-29-2	53.5-55				11.4	21.6
B-29-2	58.5-60				6.8	23.8
B-29-2	63.5-65				9.6	21.9
B-29-2	68.5-70	27	17	10	87.4	23.8
B-29-2	73.5-75	35	16	19		
B-29-2	83.5-85	38	17	21		
B-29-2	93.5-95				60.7	27.7

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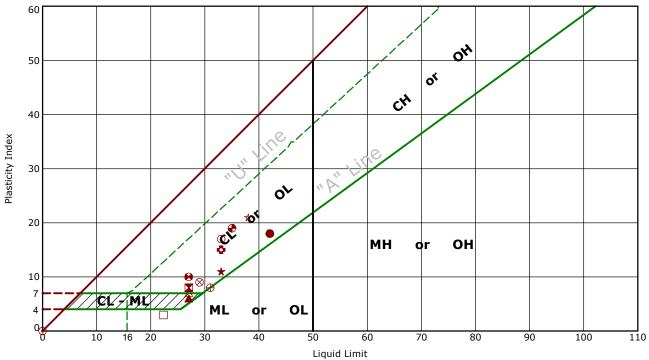
Summary of Laboratory Results

Boring ID	Depth (Ft.)	Liquid Limit	Plastic Limit	Plasticity Index	% Fines	Water Content (%)
B-29-2	98.5-100				23.5	29.1



Atterberg Limit Results

ASTM D4318

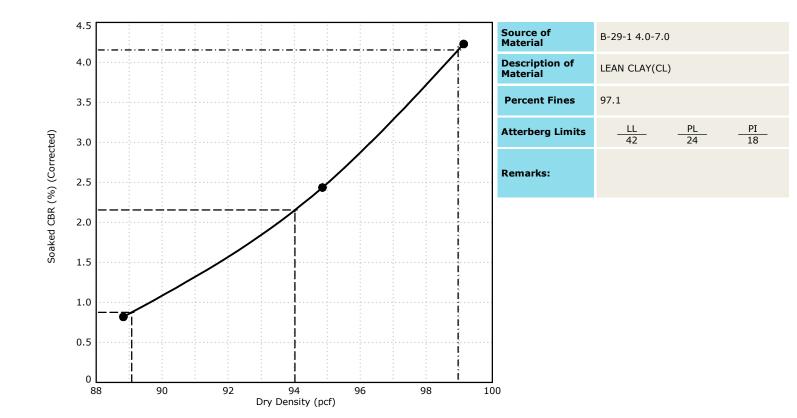


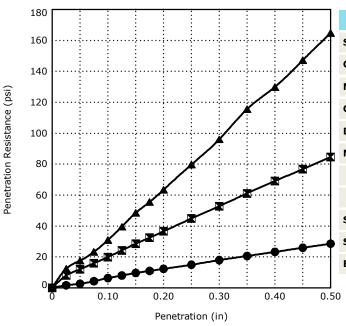
	Boring ID	Depth (Ft)	LL	PL	PI	Fines	USCS	Description
•	B-29-1	4 - 7	42	24	18	97.1	CL	LEAN CLAY
×	B-29-1	5 - 6.5	27	19	8			
•	B-29-1	7.5 - 9	27	21	6			
*	B-29-1	17.5 - 19	33	22	11	97.9	CL	LEAN CLAY
•	B-29-1	20 - 22	NP	NP	NP	94.5	ML	SILT
۰	B-29-1	68.5 - 70	33	18	15			
0	B-29-1	88.5 - 90	33	16	17			
Δ	B-29-2	5 - 6.5	27	20	7			
⊗	B-29-2	10 - 11.5	29	20	9			
Ф	B-29-2	15 - 16.5	31	23	8			
	B-29-2	20 - 22	22	19	3	97.9	ML	SILT
0	B-29-2	68.5 - 70	27	17	10	87.4	CL	LEAN CLAY
•	B-29-2	73.5 - 75	35	16	19			
*	B-29-2	83.5 - 85	38	17	21			



California Bearing Ratio

ASTM D1883-07²





Sample No.	1	2	3	
Sample Condition		Soaked		
Compaction Method ASTM 698A				
Maximum Dry Density (pcf)	98.97	98.97	98.97	
Optimum Moisture Content (%)	18.9	18.9	18.9	
Dry Density before Soaking, (pcf)	88.82	94.85	99.14	
Moisture Content, (%)				
After Compaction	19.2	19.3	19	
Top 1" After Soaking	34.7	30.5	31	
Surcharge, (lbs)	10.00	10.00	10.00	
Swell, (%)	1.24	1.52	1.86	
Bearing Ratio, (%)	0.8	2.4	4.2	

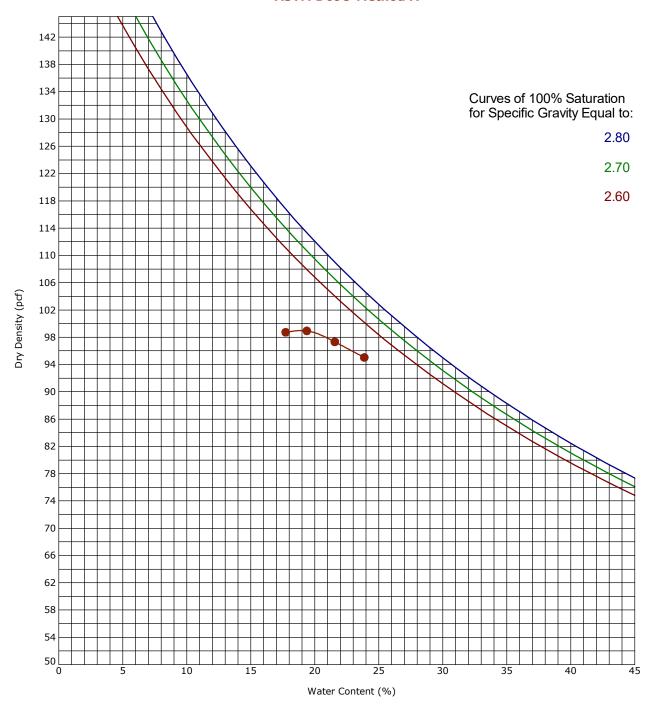
Dry Density @ 90%	89.1	pcf
Dry Density @ 95%	94.0	pcf
Dry Density @ 100%	99.0	pcf

CBR @ 90% Density	0.9
CBR @ 95% Density	2.2
CBR @ 100% Density	4.2



Moisture-Density Relationship

ASTM D698-Method A

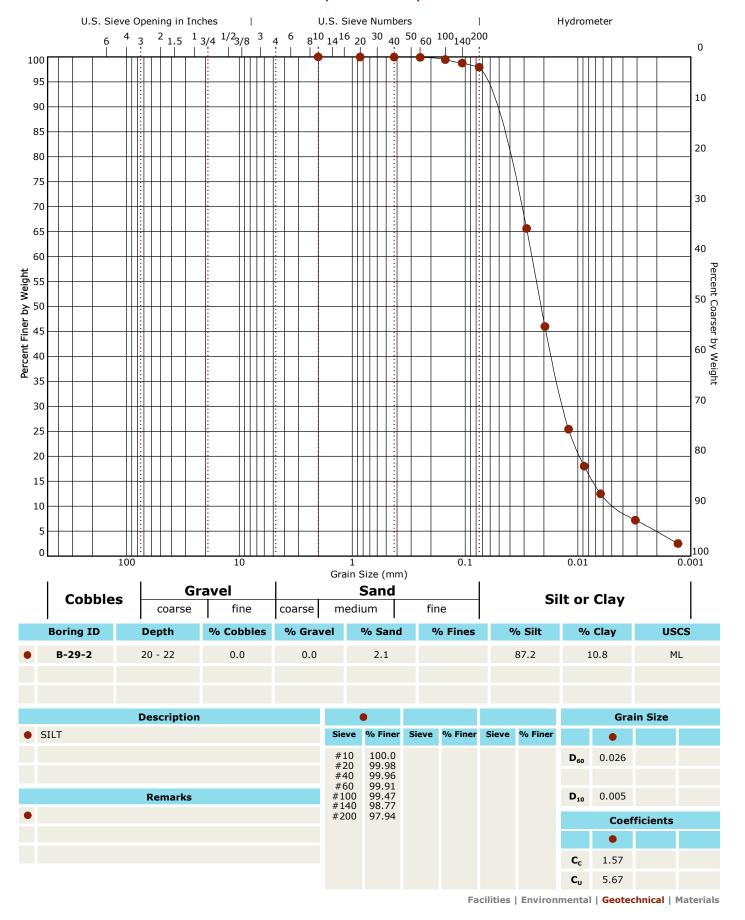


Во	oring ID	Depth	(Ft)	Description of Materials				
E	B-29-1	4 - 7		LEAN CLAY(CL)				
Fines (%)	Fraction > mm size	LL	PL	PI	I Test Method Maximum Dry Density Optimum Water Content (pcf) (%)			
97	0.0	42	24	18	ASTM D698-Method A 99.0 18.9			



Grain Size Distribution

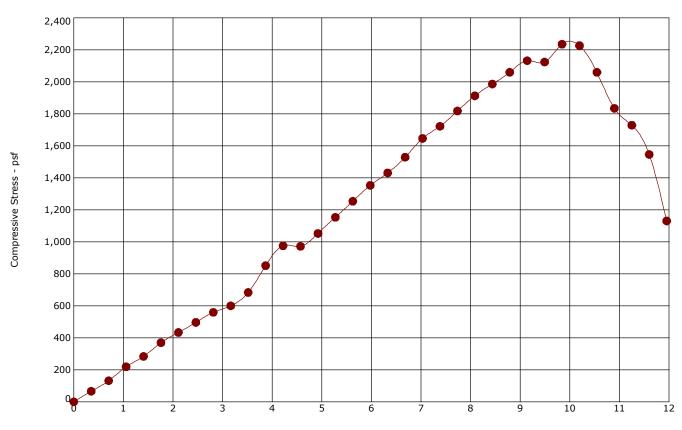
ASTM D422 / ASTM C136 / AASHTO T27



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Unconsolidated-Undrained Test ASTM D2850



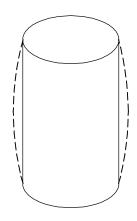
Axial	Strain	-	(%)
-------	--------	---	-----

Boring ID	Depth (Ft)	Sample type	LL	PL	PI	Fines (%)	Description
B-29-1	20 - 22	Shelby Tube	NP	NP	NP	94.5	SILT(ML)

Remarks:

Specimen	railure	моае

Specimen Test Data

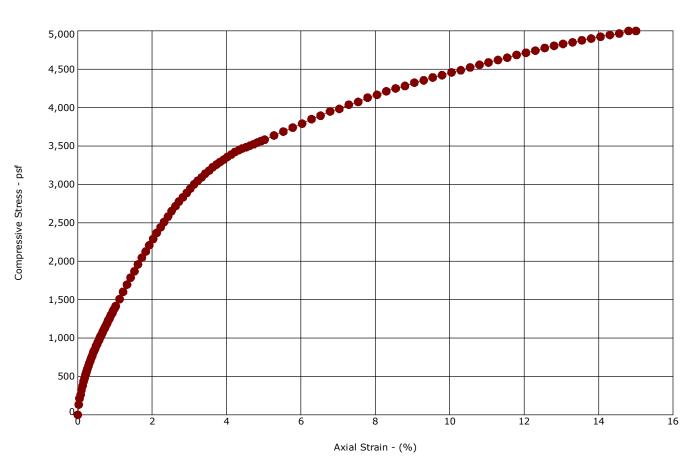


Failure Mode: Bulge (dashed)

Specimen	Test Data
Moisture Content (%):	25.2
Dry Density (pcf)	96.0
Diameter (in):	2.88
Height (in):	5.69
Height / Diameter Ratio:	1.98
Calculated Saturation (%)	92.27
Calculated Void Ratio:	0.72
Assumed Specific Gravity:	2.65
Failure Strain (%):	9.84
Compressive Strength (psf):	2235
Undrained Shear Strength (psf):	1118
Strain Rate (in/min):	
Confining Pressure (psi):	



Unconsolidated-Undrained Test ASTM D2850



Boring ID	Depth (Ft)	Sample type	LL	PL	PI	Fines (%)	Description
B-29-2	20 - 22	Shelby Tube	22	19	3	97.9	SILT(ML)

B-29-2	20 - 22	Shelby Tube	22	19	3	97.9	SILT(ML)			
Specimen Failure Mode						Specimen Test Data				
					ſ	Moisture Content	t (%):	21.3		
					ľ	Dry Density (pcf))	106.2		
					f	Diameter (in):		2.78		
					ŀ	Height (in):		5.65		
	/		1		!	Height / Diamete	er Ratio:	2.03		
	į		1		(Calculated Satur	ation (%)	97.99		
				(Calculated Void I	Ratio:	0.59			
	() 		1	Assumed Specific	c Gravity:	2.7		
	į		į		1	Failure Strain (%	b):	14.81		
	7		į		(Compressive Str	ength (psf):	4998		
\				1	Undrained Shear	Strength (psf):	2499			
					Strain Rate (in/n	nin):	0.0565			
				(Confining Pressu	re (psi):	16.0			
	Failure Mo	de: Bulge (dash	ned)		į	Remarks:				



Client

American Structurepoint Inc Cleveland, OH

Project

AltDeliv_TDOT_Bridge 33-34 1A255072

Date Received:

Corrosivity Suite - Results								
	Sample Location	B-29-1						
S	Sample Depth (ft.)	10.0-11.5'						
Acidity (pH)	AASHTO T289	7.1						
Water Soluble Sulfate Ion Content (mg/Kg)	ASTM C1580	306						
Water Soluble Sulfide Content (mg/Kg)	AWWA 4500-S,D	Nil						
Water Soluble Chloride Ion Content (mg/Kg)	ASTM D512	<20						
Oxidation-Reduction Potential (RmV)	ASTM G200	91.3						
Total Dissolved Salts (mg/Kg)	AWWA 2520 B	348						
Electrical Resistivity (Ω-cm)	ASTM G57	1800						

Verified By: Myles Warner

page 1 of 1

These tests were performed in general accordance with the applicable AASHTO, ASTM, and AWWA test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced without the full written consent of Terracon Consultants Inc.. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar materials.



Notes

- 1) The MASW arrays performed by Terracon on May 15, 2025 are shown above in **RED**. Label locations indicate the start, or "0-foot," mark of the arrays. Several geophone locations were collected using a sub-meter accurate GPS receiver.
- 2) Geotechnical boring locations were collected using a handheld GPS and are shown above in BLUE.
- 3) Aerial imagery provided by Bing.

PROJECT MANAGER:	PROJECT NUMBER:
ECC	1A255072
DRAWN BY:	DRAWING SCALE:
AGW	AS SHOWN
CHECKED BY:	FILE NAME:
NBR	Loc-29.srf
APPROVED BY:	DATE DRAWN:
DAB	8/7/2025



1922 Old Murfreesboro Pike, Suite 905 Nashville, TN 37217

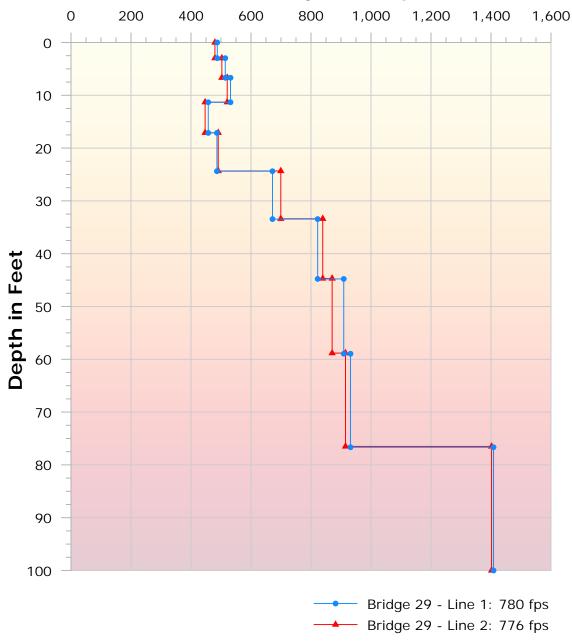
Geophysical Exploration Plan

Replacement of Bridge 29 (SR-87 Over Lagoon Creek) Haywood County, TN EXHIBIT

1

Vs100' Model TDOT Bridge 29

Shear Wave Velocity in Feet per Second



Notes:

- 1) Seismic testing was conducted by Terracon on May 15, 2025.
- 2) Shear wave velocity testing and calculations were conducted in general accordance with ASCE 7-16 and IBC 2018.

PROJECT MANAGER: PROJECT NUMBER: ECC 1A255072		Site Classification Data	EXHIBIT
DRAWN BY: PROJECT TASK: AGW 1	erracon	Replacement of Bridge 29	
CHECKED BY: FILE NAME: NBR Vs100.qpj	1922 Old Murfreesboro Pike #905	(SR-87 Over Lagoon Creek)	2
APPROVED BY: DATE: 8/7/2025	Nashville, TN 37217	Haywood County, TN	

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Supporting Information

Contents:

General Notes Unified Soil Classification System



General Notes

Sampling	Water Level	Field Tests
Grab Shelby Sample Standard Penetration Test	Water Initially Encountered Water Level After a Specified Period of Time Water Level After a Specified Period of Time Cave In Encountered Water levels indicated on the soil boring logs are the levels measured in the borehole at the times	Field Tests N Standard Penetration Test Resistance (Blows/Ft.) (HP) Hand Penetrometer (T) Torvane (DCP) Dynamic Cone Penetrometer UC Unconfined Compressive Strength
	indicated. Groundwater level variations will occur over time. In low permeability soils, accurate	(PID) Photo-Ionization Detector
	determination of groundwater levels is not possible with short term water level observations.	(OVA) Organic Vapor Analyzer

Descriptive Soil Classification

Soil classification as noted on the soil boring logs is based Unified Soil Classification System. Where sufficient laboratory data exist to classify the soils consistent with ASTM D2487 "Classification of Soils for Engineering Purposes" this procedure is used. ASTM D2488 "Description and Identification of Soils (Visual-Manual Procedure)" is also used to classify the soils, particularly where insufficient laboratory data exist to classify the soils in accordance with ASTM D2487. In addition to USCS classification, coarse grained soils are classified on the basis of their in-place relative density, and fine-grained soils are classified on the basis of their consistency. See "Strength Terms" table below for details. The ASTM standards noted above are for reference to methodology in general. In some cases, variations to methods are applied as a result of local practice or professional judgment.

Location And Elevation Notes

Exploration point locations as shown on the Exploration Plan and as noted on the soil boring logs in the form of Latitude and Longitude are approximate. See Exploration and Testing Procedures in the report for the methods used to locate the exploration points for this project. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

Strength Terms

(More than 50% reta Density determined I	Coarse-Grained Soils ined on No. 200 sieve.) by Standard Penetration istance	Consistency of Fine-Grained Soils (50% or more passing the No. 200 sieve.) Consistency determined by laboratory shear strength testing, field visual-manual procedures or standard penetration resistance				
Relative Density	Standard Penetration or N-Value (Blows/Ft.)	Consistency	Unconfined Compressive Strength Qu (psf)	Standard Penetration or N-Value (Blows/Ft.)		
Very Loose	0 - 3	Very Soft	less than 500	0 - 1		
Loose	4 - 9	Soft	500 to 1,000	2 - 4		
Medium Dense	10 - 29	Medium Stiff	1,000 to 2,000	5 - 8		
Dense	30 - 50	Stiff	2,000 to 4,000	9 - 15		
Very Dense	> 50	Very Stiff	4,000 to 8,000	16 - 30		
		Hard	> 8,000	> 30		

Relevance of Exploration and Laboratory Test Results

Exploration/field results and/or laboratory test data contained within this document are intended for application to the project as described in this document. Use of such exploration/field results and/or laboratory test data should not be used independently of this document.

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Unified Soil Classification System

Criteria for As	Soil Classification				
	Group Symbol	Group Name ^B			
	Gravels:	Clean Gravels:	Cu≥4 and 1≤Cc≤3 ^E	GW	Well-graded gravel F
	More than 50% of	Less than 5% fines ^c	Cu<4 and/or [Cc<1 or Cc>3.0] E	GP	Poorly graded gravel F
	coarse fraction retained on No. 4	Gravels with Fines:	Fines classify as ML or MH	GM	Silty gravel F, G, H
Coarse-Grained Soils:	sieve	More than 12% fines c	Fines classify as CL or CH	GC	Clayey gravel F, G, H
More than 50% retained on No. 200 sieve		Clean Sands:	Cu≥6 and 1≤Cc≤3 ^E	SW	Well-graded sand ^I
	Sands: 50% or more of coarse fraction passes No. 4 sieve	Less than 5% fines D	Cu<6 and/or [Cc<1 or Cc>3.0] E	SP	Poorly graded sand ^I
		Sands with Fines:	Fines classify as ML or MH	SM	Silty sand G, H, I
		More than 12% fines D	Fines classify as CL or CH	SC	Clayey sand G, H, I
		Inorganic:	PI > 7 and plots above "A" line ¹	CL	Lean clay K, L, M
	Silts and Clays:	inorganic.	PI < 4 or plots below "A" line ³	ML	Silt K, L, M
	Liquid limit less than 50	Organic:	$\frac{LL \ oven \ dried}{LL \ not \ dried} < 0.75$	OL	Organic clay K, L, M, N
Fine-Grained Soils: 50% or more passes the		Organic.	$LL \ not \ dried < 0.75$	OL	Organic silt K, L, M, O
No. 200 sieve		Inorganic:	PI plots on or above "A" line	CH	Fat clay K, L, M
	Silts and Clays: Liquid limit 50 or	inorganic.	PI plots below "A" line	MH	Elastic silt K, L, M
	more	Organic:	LL oven dried	ОН	Organic clay K, L, M, P
		Organic:	$\frac{LL \text{ oven arrea}}{LL \text{ not dried}} < 0.75$	OH	Organic silt ^{K, L, M, Q}
Highly organic soils:	Primarily	organic matter, dark in o	color, and organic odor	PT	Peat

- A Based on the material passing the 3-inch (75-mm) sieve.
- B If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.
- ^c Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.
- P Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with silt, SP-SC poorly graded sand with clay.

E Cu =
$$D_{60}/D_{10}$$
 Cc = $\frac{(D_{30})^2}{D_{10} \times D_{60}}$

- $^{\mathsf{F}}$ If soil contains ≥ 15% sand, add "with sand" to group name.
- ^G If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

- H If fines are organic, add "with organic fines" to group name.
- If soil contains \geq 15% gravel, add "with gravel" to group name.
- J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.

 K If soil contains 15 to 20% plus No. 200, add "with sand" or
- K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.
- $^{\text{L}}$ If soil contains \geq 30% plus No. 200 predominantly sand, add "sandy" to group name.
- ^M If soil contains ≥ 30% plus No. 200, predominantly gravel, add
 "gravelly" to group name.
- N PI ≥ 4 and plots on or above "A" line.
- PI < 4 or plots below "A" line.
- P PI plots on or above "A" line.
- Q PI plots below "A" line.

